

Operational Impact of Delay/Rate Problems

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This document looks at the effect of the known problems encountered when the *a priori* delay on a specific baseline is close to zero or an appropriate number of tape-frame lengths, or when the *a priori* delay-rate is close to zero. The first part reviews formulations for the occurrence of these conditions, as confirmed empirically over the last few experiments. The second part show results from these experiments graphically, to provide a feel for the impact of these problems in a small number of specific (actual) cases. The third part simulates the percentage of data affected by the full EVN on a variety of source δ 's, sub-band bandwidths, fan-outs, integration times, and frequencies. This paper can be found on the public ftp site under `.../rmc/dlyrt0.ps.gz` or through my web page `www.jive.nl/~campbell`.

1. Basic Rules, Pattern Recognition

The delay-based problem occurs when tape headers from the two data streams composing the baseline start to overlap with each other. This is a concern only for MkIV–MkIV baselines; baselines having one or more VLBA recorder will not be affected. This condition pertains when the *a priori* delay is within $\pm t_{\text{crit}}$ of nT_{frm} , where $n = 0, \pm 1, \pm 2, \dots$. Equations that seem to work predictively are:

$$t_{\text{crit}} = \frac{(160 + N_{\text{lag}}/2) \cdot M_{\text{fanout}}}{2BW} \quad (1)$$

$$T_{\text{frm}} = \frac{2 \times 10^4 \cdot M_{\text{fanout}}}{2BW}, \quad (2)$$

where 160 is the header size in bits and 2×10^4 is the tape-frame size in bits. The fan-out factor is required to obtain the total number of bits in the combined data stream, and the bandwidth factor converts delays from lag-units to physical time units. Something to keep in mind for §3 is that narrower sub-band bandwidths and higher fan-outs will increase t_{crit} linearly — especially important around the $n = 0$ “lobe”, since the higher-order lobes will also be pushed outwards. Figure 1 shows typical amplitude and phase *vs.* time response for one of these delay instances (from EP027B). The affected baseline is On–Wb; On–Ef is provided as a control showing the Reference-Target nature of these phase-reference observations. The amplitude during the event (0807–0813 UT) shows a characteristic “double-trapezoid” response, and the phase a characteristic flat $\varphi \simeq +140^\circ$ or -40° trace

(shifting by the 180° during the minimum of the “double-trapezoid”. Note that this event started in the reference source & continued during the following program source scan. This pass was picked to show that the net behavior is unaffected by the source change, although you can see a little more structure during the bright-source portion.

The delay-rate-based problem occurs when the *a priori* fringe rotator makes only a small number of wraps within an integration period. From looking at the range over which the fringe amplitude was affected on a few instances, the following formulation appears safe:

$$|\text{Rate}| \leq \frac{3}{t_{\text{int}} \cdot \nu_0}. \quad (3)$$

For most cases, “2” in the numerator also suffices. The frequency dependence will result in slightly different ranges for different sub-bands, which could become somewhat significant for dual-frequency observations (or others with non-contiguous bands, say for single-band frequency-synthesis experiments or those trying to be especially clever about Faraday rotation or ionospheric delay). Figure 2 shows typical amplitude *vs.* time response for these delay-rate instances (this time from EP027A). The affected baseline is Nt–Ef; Wb–Ef is provided as a control. We can see separate events for both the reference and target sources (showing the effect of slightly different positions: reference $\alpha = 12^{\text{h}}15^{\text{m}}03^{\text{s}}.9781; = 16^\circ54'37''.936$, target $\alpha = 12^{\text{h}}18^{\text{m}}50^{\text{s}}.0; = 14^\circ24'53''$). The amplitude of both events shows a clear spike.

The relevant formulae for *a priori* delay and delay rate are:

$$\tau = \frac{-B}{c} [\cos \delta_b \cos \delta_s \cos (\alpha_b(t) - \alpha_s) + \sin \delta_b \sin \delta_s] \quad (4)$$

$$\frac{\partial \tau}{\partial t} = \frac{B\Omega_\oplus}{c} \cos \delta_b \cos \delta_s \sin (\alpha_b(t) - \alpha_s). \quad (5)$$

Subscripts *b* and *s* refer to the baseline and source, respectively. *B* is the baseline length. The key point from these equations is that the sinusoidal variation of delay and delay-rate will be smaller for shorter baselines; these will hence spend more time in the relevant Δt ranges in which the above problems will occur. The worst of all cases would be something like Wb–Ef in a UHF experiment with narrow sub-band bandwidths and high fan-out.

Amplitude for pass23

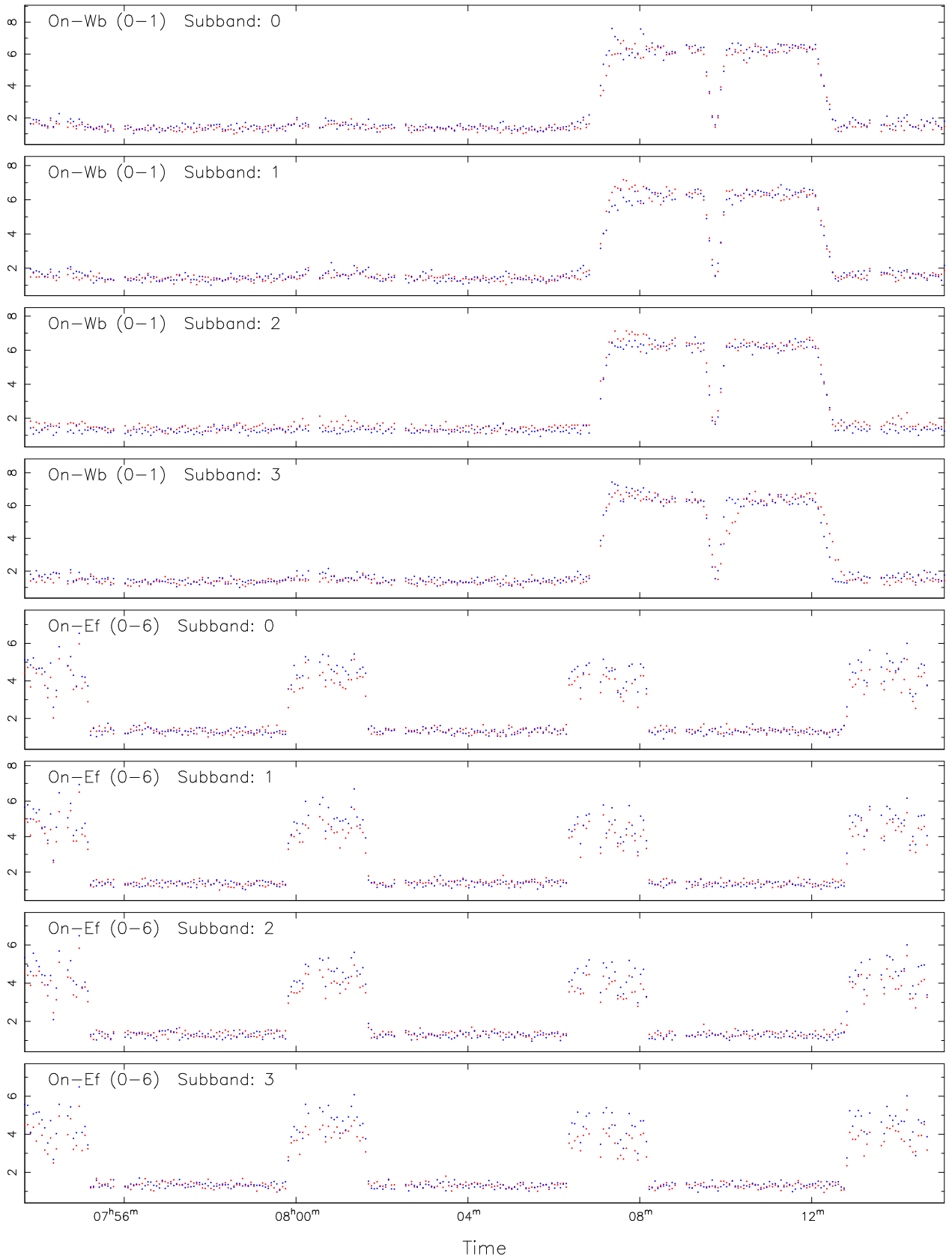


Fig. 1a: Amplitude *vs.* time during a delay=0 event.

Phase for pass23

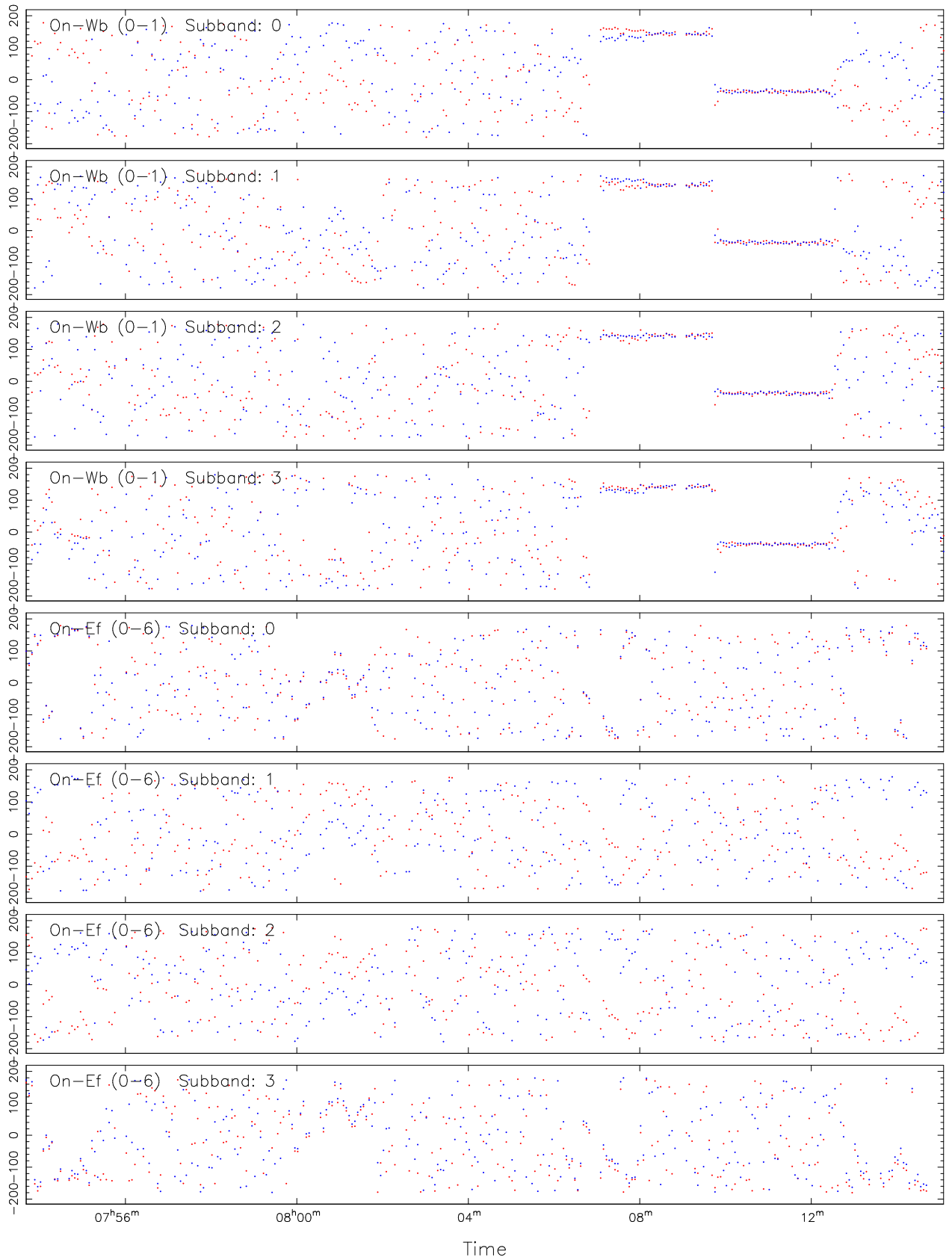


Fig. 1b: Phase *vs.* time during a delay=0 event.

Amplitude for pass17

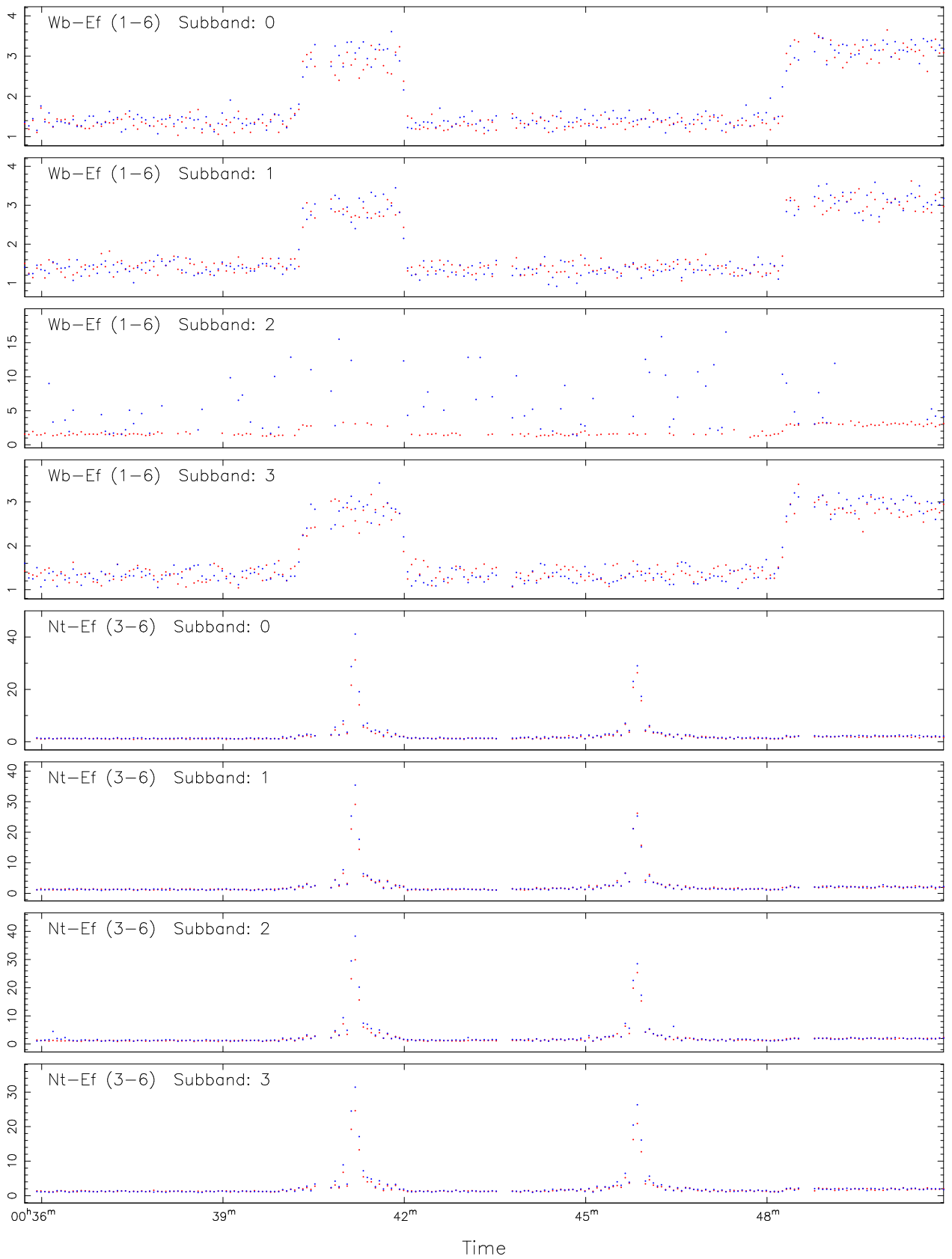


Fig. 2: Amplitude *vs.* time during a delay-rate=0 event.

2. Results from Actual Experiments

Figure 3 shows delay and rate calculations for some baselines (one-third) for both sources from ES030A, color coded as annotated. This was a phase-reference experiment of Cyg X-1 (target) and 1955 (reference). It used 8 MHz sub-bands and fan-out of 2:1. The vertical dotted lines denote the beginning of passes. The horizontal lines in delay plots (left column) show $\pm t_{\text{crit}}$ of $n \cdot T_{\text{frm}}$, as from equations (1)–(2). These lines are dashed if involving a VLBA station (*i.e.*, not actually relevant). The horizontal line in the rate plots (right column) marks zero. The source-curves were obtained by the (old) `CALC8.1/dcalc` method; `dcalc` output was read into, baselines formed in, and plotted from IDL. We see the delay problem whenever the curves enter the “danger zones”. I’ve been using such plots to see where to investigate the data for the delay and rate problems in actual experiments — finding problems in these plots or in `fplots/tplots` in `aips++` seems entirely reflexive: nothing seems missed either way you proceed (though sometimes the `rate=0` problem doesn’t leave an obvious trace in `fplot` lag-amplitude plots).

Note that in Wb–Ef we can see the effect of the delay problem first in Cyg X-1 and then later in the reference source 1955. This is confirmed by `tplots`. There’s no delay problem for Wb–On during this experiment because during the observed UT range the delay is never close to a “lobe” (0 or $-2500 \mu\text{s}$). On longer baselines (say Wb–Nt), a source may see more than one “lobe”, but generally spend less time sweeping through each.

As a general rule, the delay problems last a few minutes (5–8), but somewhat longer on the shortest baselines (Ef–Wb, Wb–Jb) when they can start to stretch on for up to ~ 20 min. The rate problems come and go within 90–120 seconds. However, as §3 will discuss, these numbers can get much worse for narrower sub-band bandwidths and higher fan-outs.

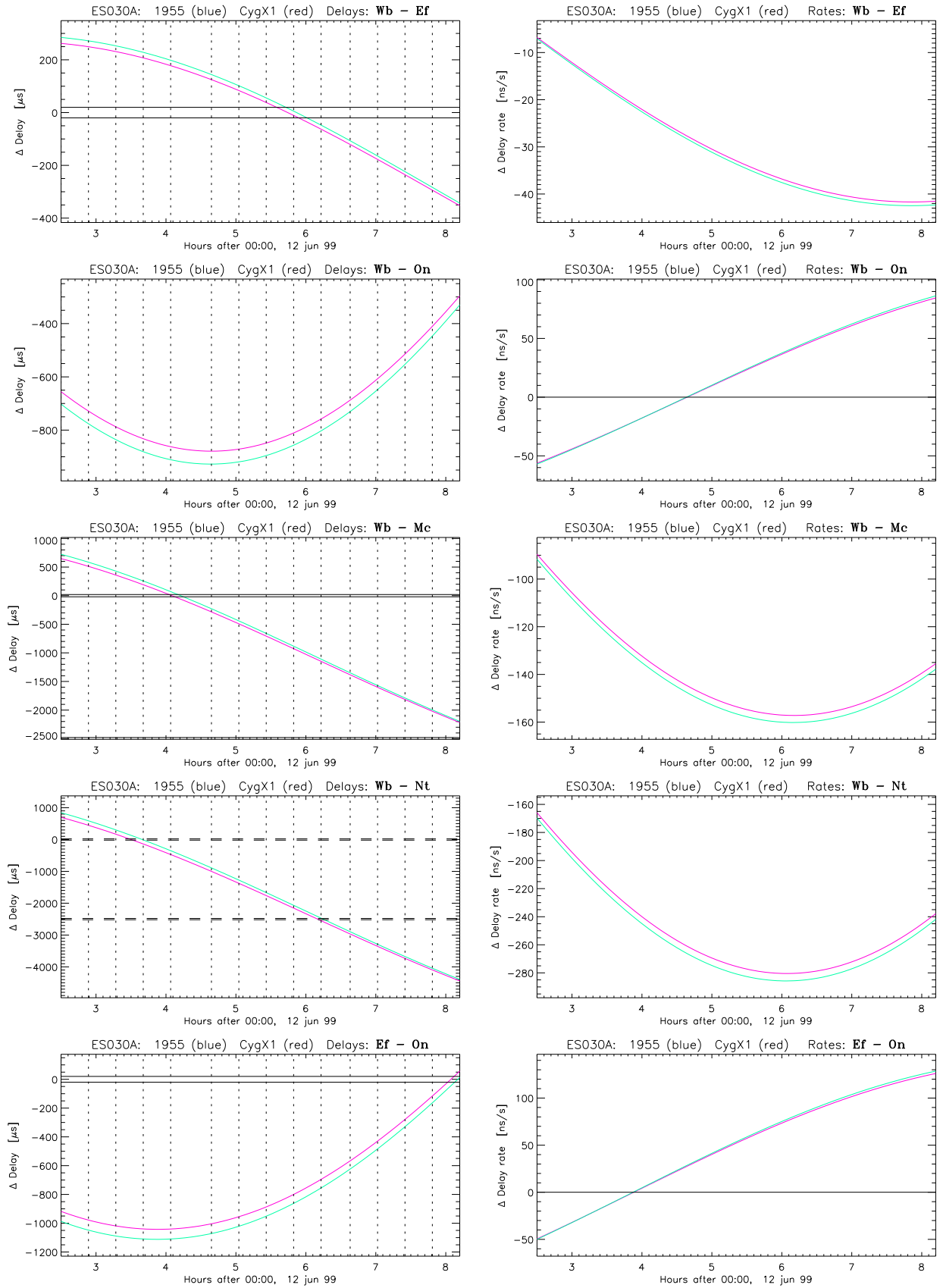


Fig. 3b: Delay and Rate *a priori* models for ES030A.

Figure 4 shows delay and rate calculations for some baselines for both sources from C99C3, color coded as annotated. This experiment used 2 MHz sub-bands and no fan-out. These two sources are unrelated, and not doing phase referencing. 13-minute scans were made every 40 minutes. The vertical dotted lines shows the boundaries of the scans. Each scan sat on only one of the sources for the full 13 minutes; the observed source is denoted by the darkening of the appropriate delay curve during specific scans.

Picking the “right” (or “wrong”) source, either by design or inadvertently, can effect the operational impact of these delay/rate problems. On Wb–Ef, pass 5, BL Lac (blue) is in the “danger zone”, but they were observing 0059 — no harm, no foul. However, on Jb–On during pass 9, BL Lac was in the “danger zone” and it was being observed. We can also see, due to the limited-duration of these problems (on all but the shortest baselines), that a non-continuous experiment could also get lucky by missing a delay/rate-crossing zero because it falls outside scan boundaries — such as Jb–Mc between passes 5 and 6 for 0059. On Jb–Sh, we can see the effect of long baselines allowing more “lobes” to come into play (of course, ignoring the fact that Sh has a VLBA recorder).

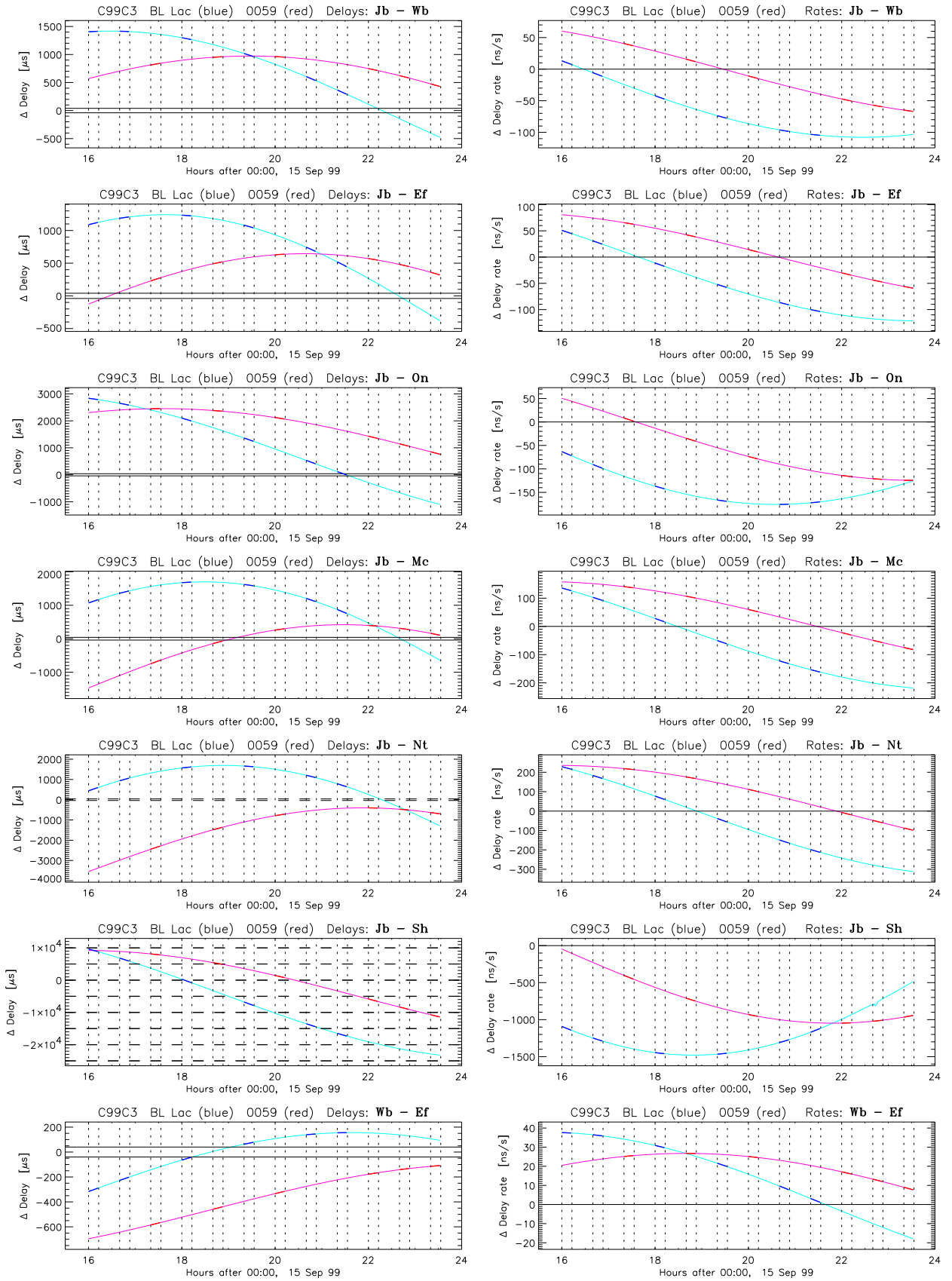


Fig. 4a: Delay and Rate *a priori* models for C99C3.

Figure 5 shows delay and rate calculations some baselines (two-thirds) for EP027A. This used 8 MHz sub-bands and fan-out of 2:1. This experiment was a phase-referencing one, but one that changed target-reference pairs quite often (up to every 22-min pass). I calculated/plotted only the delay/rate curves reference source for the duration of each pass. As can be seen from the ES030A plots in Fig. 3, there will be some offset between the plotted curves and those for the target sources, depending on the relative positions of the two. Such differences are ignored in these plots, affecting to some degree their predictive power when applied blindly. Use of actual polynomials from the correlator will solve this sort of problem. Because of all the source-pair changes, the delay/rate curves are quite jumpy; the vertical offsets correspond to the source changes. The portions of the curves in red correspond to times when problems at On or Mc caused data loss.

In Fig. 5a, we can see an unlucky sequence of source changes in On–Jb between around 0100–0430 UT, where the source changes keep the delay fairly well centered on the $-1T_{\text{frm}}$ “lobe” (irrelevant in practice, of course, since there’s no data on On during this time). There are no major problems on other baselines (On–Wb has delay problems in the first two passes after On comes on-line). You can get an idea of the precision with which these kind of plots can predict delay problems by looking at Wb–Ef in Fig. 5b. There are two scans very close to the upper boundary of the “danger zone” around 0600UT. In the first instance, you can see the effect of the trailing edge of the delay problem during the first minute or so of the pass. (During the second instance, Ef didn’t head peak [as it didn’t for any of the first two reverse passes for the tapes in this experiment], so the possible problem was moot.)

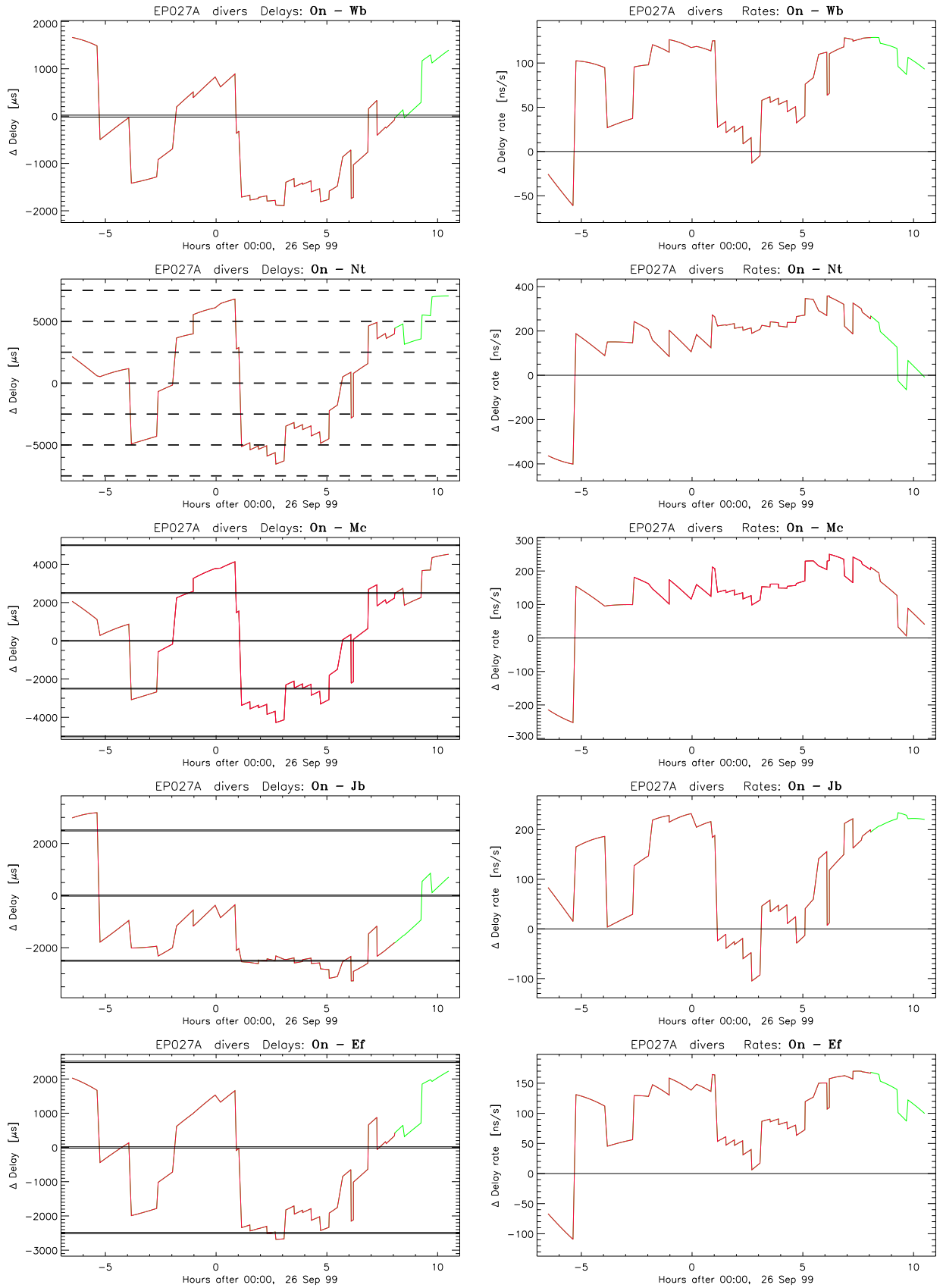


Fig. 5a: Delay and Rate *a priori* models for EP027A.

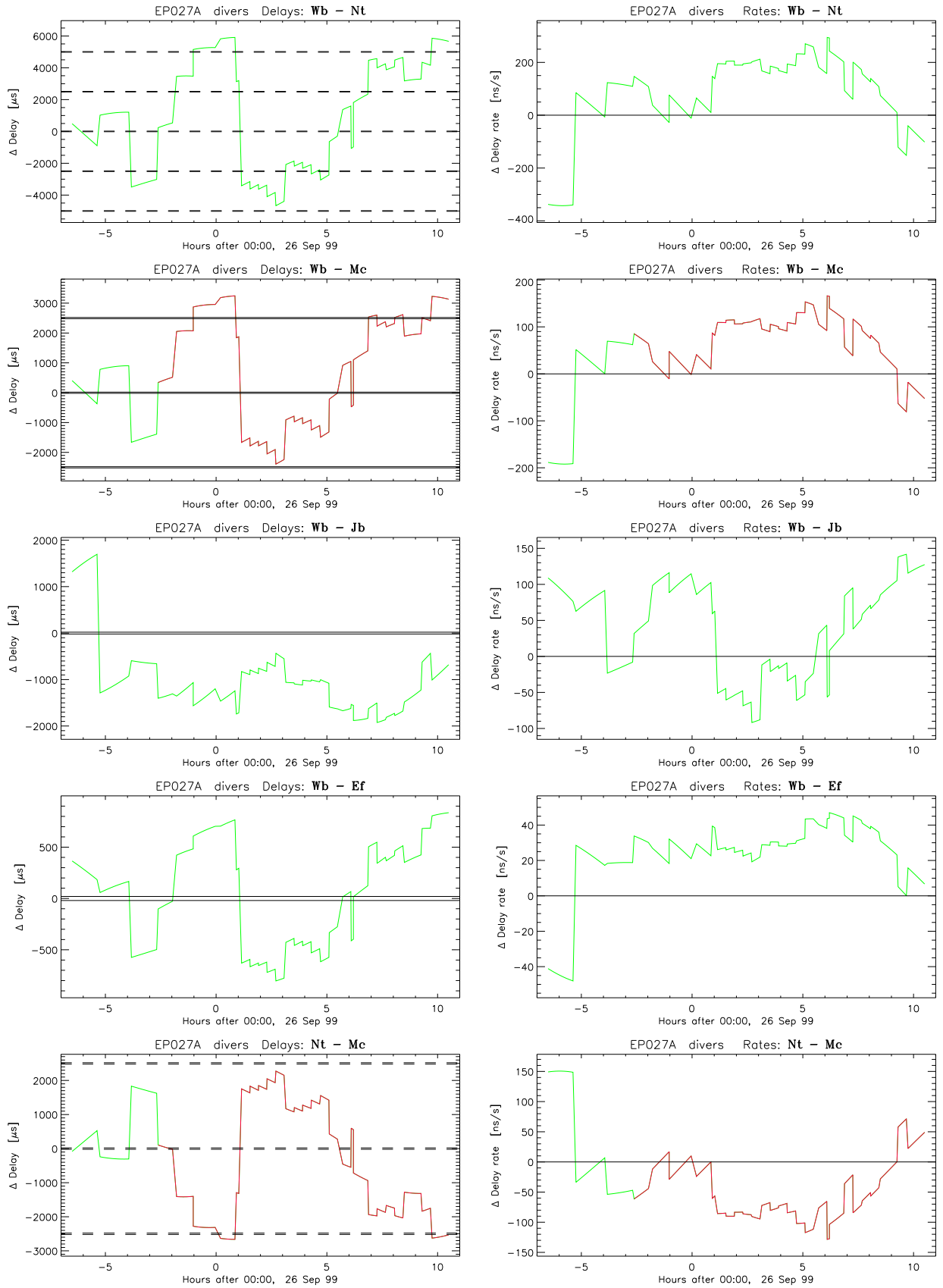


Fig. 5b: Delay and Rate *a priori* models for EP027A.

Figure 6 shows delay and rate calculations for EP027B. In many ways this plot is similar to that for EP027A, except here Jb was missing altogether, and there weren't any problems with On or Mc. In On–Ef, the observations were scheduled such that they just missed any effect from the $-1T_{\text{frm}}$ “lobe” from 0200–0500UT, as opposed to in EP027A (Fig. 5a).

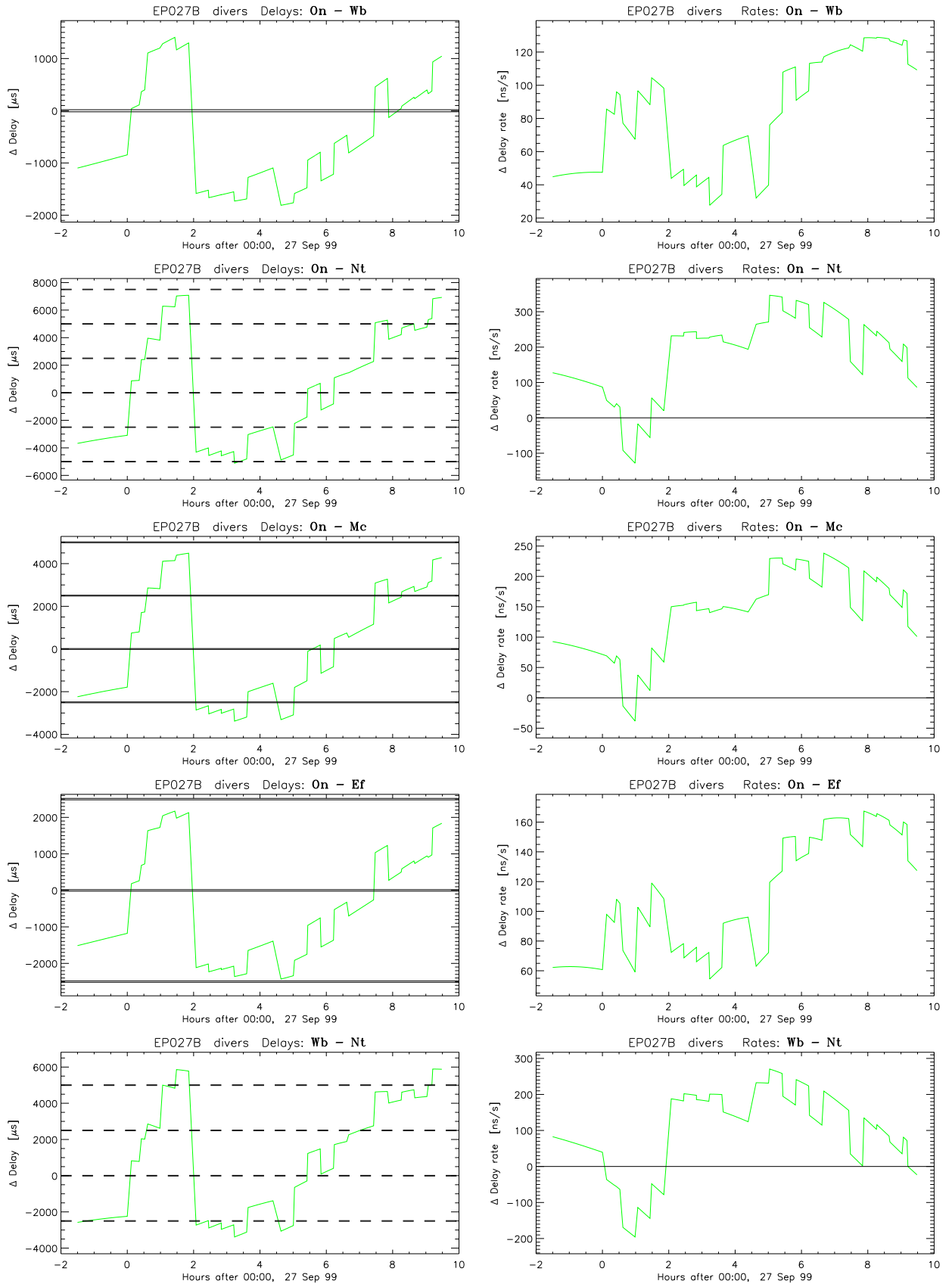


Fig. 6a: Delay and Rate *a priori* models for EP027B.

3. Simulation of the Delay/Rate Problems

The above plots show illustrative examples of the occurrences of the delay and rate problems drawn from actual experiments. You can get a feel for the amount of data lost to the delay and rate problems by seeing for what fraction of the total observing time the delay/rate curves lie within the “danger zones.” We can also run simulations of a full sidereal-day observation of a specific source from the full EVN to get a more quantitative value of the amount good data remaining after the delay and rate problems take their tolls. This will also allow us to summarize how various observing parameters (sub-band bandwidth, fan-out, frequency, integration time) affect the data loss. The following six pages show the result of such simulations: the first two a delay simulation for EVN stations ever having Mk IV formatters in the past few sessions, and the last four a rate simulation for the full EVN.

The delay simulation considers three different sub-band bandwidths (8, 2, 0.5 MHz), three different fan-outs (1:1, 1:2, 1:4), and three different N_{lag} configurations (32, 128, 512) — some combinations of all three parameters may not actually exist. The rate simulation considers three different observing frequencies (329MHz, 1.6GHz, 22GHz) and two different integration times (1, 4 s). Both consider source declinations ranging from $+80^\circ$ to -20° in steps of 20° . At the top of the tables are listed the relevant parameters from equations (1)–(3) resulting from combinations of the appropriate “experimental” parameters. We follow each of the sources (at the different declinations) for a full sidereal day (sampled every 4 [UT]s), and keep track of those times for which it is up. (Since a full sidereal day is being followed, the RA of the source is irrelevant; it wound up being set at 0^{h} by omission.) The first column in the tables is the baseline, the second is the amount of time the source is up on the baseline.

- The remainder of the columns of the delay simulation table contain the percentage of time for which the source is up that it is unaffected by the delay problem, truncated down to the next lowest percent. Each of these columns belongs to one of the possible sub-band/fan-out/ N_{lag} combinations as labeled in the column headings.
- In the rate simulation table, the next nine columns pertain to a delay simulation done without consideration of the N_{lag} factor, and should be ignored. The next two columns give the maximum and minimum delay for all times for which the source is up on the baseline (for which there wasn’t room in the new delay-simulation table). The remainder of the columns relate to the rate problem. The next six columns contain the percentage of time for which the source is up that it is unaffected by the rate problem, and the last two columns give the maximum and minimum rates seen by the baseline while the source is up.

All delays in the tables are in [μs], and all rates in [ns/s].

A couple quick examples from the tables, and then you're on your own to read/interpret as you see fit for your favorite observing set-up/region of the sky (or let me know if you'd want something more specific). The keys to understanding the percentage numbers for delays involves the interplay among the minimum & maximum delays and the spacing & width of the "danger zones." The typical response is to have more data loss as the bandwidth decreases, the fan-out increases, and/or the N_{lag} increases.

- There's a sudden drop off in Ef–Wb in $BW = 0.5\text{ MHz}$ and fan-out=1:4 for $\delta = 80^\circ$, even for the smallest N_{lag} . This comes about because Ef–Wb's total spanned delay (-418 to $-662\ \mu\text{s}$ from columns 12–13 in the 2nd table) lies well outside any "danger zone" until this BW/fan-out combination which pushes the width of the $n = 0$ lobe up to $\pm 704\ \mu\text{s}$ (for $N_{\text{lag}} = 32$).
- By comparison, the delay for Wb–Jb $\delta = 80^\circ$ crosses zero, so is more gradually affected by the increase in the width of the 0th lobe (until it mostly loses **all** data by 0.5 MHz).
- Check out Jb–Mc (still $\delta = 80^\circ$) using 8 MHz sub-bands for a counter-example. Here, the its delay-range (1203 to $2651\ \mu\text{s}$) crosses two "danger zones" in the 8MHz/1:1 case (at 1250 & $2500\ \mu\text{s}$), but none in the 8MHz/1:4 case (first comes at $5000\ \mu\text{s}$).
- As the source declination changes, the range of delays also changes (eq. 4), with corresponding effect on these sorts of arguments.

Similar points apply to the rate tables. Here, the only egregious losses are in Ef–Wb at 1s integration period at L-band and below, and all baselines for the most northerly declinations at 329 MHz. Again, the problem is the reduced amplitude of the rate sinusoid (eq. 5) in relation to the size of the "danger zone" (the rate sinusoid is symmetric about 0, so the possibility of missing the zero-crossing doesn't arise as it does for delays). Especially for the rate data, remember how the percentages were truncated; a "99" could result from as little as 1 4-s sample out of 21554 falling into a "danger zone."

As presented, the delay and rate portions of the tables are independent; both give the percentage of good data out of the possible data (*i.e.*, when the source is up on a given baseline). The net data loss due to both errors would be at most the sum of the loss due to each. Individual UTs that are lost due to both would be double counted.

COMBINATIONS CONSIDERED

--- Delay: frame size/header size [us] ---

8MHz: 1:1 1250/10 1:2 2500/20 1:4 5000/40
2MHz: 1:1 5000/40 1:2 10000/80 1:4 20000/160
0.5MHz: 1:1 20000/160 1:2 40000/320 1:4 80000/640

Lags: 32, 128, 512

**** Source declination = +80 ****

Table with columns for frequency bands (8MHz, 2MHz, 0.5MHz) and sub-bands (up, 1:1, 1:2, 1:4). Rows list various combinations like Ef-Wb, Ef-On, etc.

**** Source declination = +60 ****

Table with columns for frequency bands (8MHz, 2MHz, 0.5MHz) and sub-bands (up, 1:1, 1:2, 1:4). Rows list various combinations like Ef-Wb, Ef-On, etc.

**** Source declination = +40 ****

Table with columns for frequency bands (8MHz, 2MHz, 0.5MHz) and sub-bands (up, 1:1, 1:2, 1:4). Rows list various combinations like Ef-Wb, Ef-On, etc.

COMBINATIONS CONSIDERED

```

--- Delay: frame size/header size [us] ---
  8MHz: 1:1 1250/ 10    1:2 2500/ 20    1:4 5000/ 40
  2MHz: 1:1 5000/ 40    1:2 10000/ 80   1:4 20000/160
  0.5MHz: 1:1 20000/160 1:2 40000/320   1:4 80000/640
  
```

```

--- Rate: proximity to 0 [ns/s] ---
  329MHz: 1s 9.119    4s 2.280
  1.6GHz: 1s 1.875    4s 0.469
  22GHz : 1s 0.136    4s 0.034
  
```

**** Source declination = +80 ****

	%	8MHz			2MHz			0.5MHz			delay		329MHz		1.6GHz		22GHz		rate	rate
		up	1:1	1:2	1:4	1:1	1:2	1:4	1:1	1:2	1:4	max	min	1s	4s	1s	4s	1s	4s	max
Ef-Wb	100.0	100	100	100	100	100	100	100	100	19	-418	-662	00	83	86	96	99	99	9	-9
Ef-On	100.0	98	100	100	100	100	100	100	100	100	-1070	-1882	80	95	95	98	99	99	30	-30
Ef-Jb	100.0	100	100	100	100	100	100	100	76	47	-219	-1002	79	94	95	98	99	99	29	-29
Ef-Cm	100.0	100	100	100	100	100	76	76	55	12	-85	-663	71	93	94	98	99	99	22	-22
Ef-Mc	100.0	98	100	100	100	100	100	100	100	100	1670	964	76	94	95	98	99	99	26	-26
Ef-Nt	100.0	99	100	100	100	100	100	100	100	100	4305	2882	88	97	97	99	99	99	52	-52
Ef-Tr	100.0	100	100	100	100	100	83	83	68	46	-96	-1064	83	95	96	99	99	99	36	-36
Ef-Sh	100.0	97	96	95	95	94	100	100	100	100	9997	679	98	99	99	99	99	99	340	-340
Ef-Ro	100.0	99	98	100	100	100	100	100	100	100	3261	1898	88	97	97	99	99	99	50	-50
Wb-On	100.0	96	100	100	100	100	100	100	100	91	-628	-1242	73	93	94	98	99	99	23	-23
Wb-Jb	100.0	98	96	92	92	84	68	68	24	00	277	-418	76	94	95	98	99	99	26	-26
Wb-Cm	100.0	96	93	87	87	71	50	50	30	00	429	-96	68	92	93	98	99	99	20	-20
Wb-Mc	100.0	100	100	100	100	100	100	100	100	100	2316	1399	82	95	96	99	99	99	34	-34
Wb-Nt	100.0	99	100	100	100	100	100	100	100	100	4952	3316	90	97	97	99	99	99	60	-60
Wb-Tr	100.0	98	97	94	94	88	77	77	50	00	424	-503	82	95	96	99	99	99	34	-34
Wb-Sh	100.0	98	98	98	98	97	100	100	100	100	10449	1308	98	99	99	99	99	99	334	-334
Wb-Ro	100.0	96	97	100	100	100	100	100	100	100	3874	2367	89	97	97	99	99	99	55	-55
On-Jb	100.0	98	100	100	100	100	100	100	91	63	1431	299	85	96	97	99	99	99	42	-42
On-Cm	100.0	98	100	100	100	100	100	100	100	84	1622	582	84	96	96	99	99	99	38	-38
On-Mc	100.0	98	97	100	100	100	100	100	100	100	3436	2149	87	96	97	99	99	99	47	-47
On-Nt	100.0	99	98	97	97	100	100	100	100	100	6042	4097	91	97	98	99	99	99	71	-71
On-Tr	100.0	100	100	100	100	100	100	100	100	77	1230	561	75	94	95	98	99	99	25	-25
On-Sh	100.0	98	98	98	98	98	100	100	100	100	11078	2550	98	99	99	99	99	99	311	-311
On-Ro	100.0	98	97	94	94	100	100	100	100	100	5113	2997	92	98	98	99	99	99	78	-78
Jb-Cm	100.0	100	100	100	100	100	75	75	21	00	344	129	00	81	84	96	98	99	8	-8
Jb-Mc	100.0	96	97	100	100	100	100	100	100	100	2651	1203	88	97	97	99	99	99	53	-53
Jb-Nt	100.0	98	98	96	96	100	100	100	100	100	5274	3134	92	98	98	99	99	99	78	-78
Jb-Tr	100.0	99	98	96	96	93	87	87	73	41	835	-774	90	97	97	99	99	99	59	-59
Jb-Sh	100.0	98	98	98	98	97	100	100	100	100	10712	1186	98	99	99	99	99	100	348	-348
Jb-Ro	100.0	97	100	100	100	100	100	100	100	100	3797	2583	86	96	97	99	99	99	45	-45
Cm-Mc	100.0	98	100	100	100	100	100	100	100	100	2308	1074	87	96	97	99	99	99	45	-45
Cm-Nt	100.0	99	100	100	100	100	100	100	100	100	4932	3003	91	97	98	99	99	99	71	-71
Cm-Tr	100.0	99	98	96	96	92	85	85	69	29	519	-932	88	97	97	99	99	99	53	-53
Cm-Sh	100.0	98	98	98	98	97	100	100	100	100	10469	956	98	99	99	99	99	99	347	-347
Cm-Ro	100.0	98	96	100	100	100	100	100	100	100	3532	2376	86	96	97	99	99	99	43	-43
Mc-Nt	100.0	97	95	100	100	100	100	100	100	100	2637	1917	77	94	95	98	99	99	27	-27
Mc-Tr	100.0	100	100	100	100	100	100	100	100	100	-1389	-2405	84	96	96	99	99	99	38	-38
Mc-Sh	100.0	97	98	98	98	97	95	95	91	81	8774	-731	98	99	99	99	99	100	347	-347
Mc-Ro	100.0	99	100	100	100	100	100	100	100	79	2038	488	89	97	97	99	99	99	57	-57
Nt-Tr	100.0	98	100	100	100	100	100	100	100	100	-3420	-4927	89	97	97	99	99	99	55	-55
Nt-Sh	100.0	98	98	98	98	98	97	97	95	91	6645	-3156	98	99	99	99	99	99	358	-358
Nt-Ro	100.0	99	100	98	98	90	83	83	75	62	-38	-1989	91	97	98	99	99	99	72	-72
Tr-Sh	100.0	98	97	97	97	95	100	100	100	100	10167	1670	98	99	99	99	99	99	310	-310
Tr-Ro	100.0	98	98	100	100	100	100	100	100	100	4314	2006	93	98	98	99	99	99	85	-85
Sh-Ro	100.0	97	97	98	98	98	97	97	95	90	2562	-8079	98	99	99	99	99	99	388	-388

*** Source declination = +20 ***

Table with columns: %, 8MHz (1:1, 1:2, 1:4), 2MHz (1:1, 1:2, 1:4), 0.5MHz (1:1, 1:2, 1:4), delay (max, min), 329MHz (1s, 4s), 1.6GHz (1s, 4s), 22GHz (1s, 4s), rate (max, min). Rows list various stations like Ef-Wb, Ef-On, Ef-Jb, etc.

*** Source declination = 0 ***

Table with columns: %, 8MHz (1:1, 1:2, 1:4), 2MHz (1:1, 1:2, 1:4), 0.5MHz (1:1, 1:2, 1:4), delay (max, min), 329MHz (1s, 4s), 1.6GHz (1s, 4s), 22GHz (1s, 4s), rate (max, min). Rows list various stations like Ef-Wb, Ef-On, Ef-Jb, etc.

**** Source declination = -20 ****

	%	8MHz			2MHz			0.5MHz			delay		329MHz		1.6GHz		22GHz		rate	rate
		up	1:1	1:2	1:4	1:1	1:2	1:4	1:1	1:2	1:4	max	min	1s	4s	1s	4s	1s	4s	max
Ef-Wb	34.1	100	100	100	100	100	100	100	99	73	845	307	82	95	96	99	99	99	48	-33
Ef-On	30.9	97	95	100	100	100	100	100	100	100	2707	1530	94	98	98	99	99	99	121	-142
Ef-Jb	32.2	98	99	98	98	96	92	92	84	69	2258	-1162	100	100	100	100	100	100	155	39
Ef-Cm	33.2	98	98	97	97	95	90	90	80	59	1598	-1049	100	100	100	100	100	100	114	38
Ef-Mc	35.5	98	99	98	98	96	92	92	84	75	384	-2364	94	98	98	99	99	99	29	-139
Ef-Nt	35.5	96	94	91	91	98	96	96	92	88	296	-5096	97	99	99	99	99	99	70	-281
Ef-Tr	31.5	98	97	98	98	96	93	93	87	78	2818	-448	95	98	98	99	99	99	31	-191
Ef-Sh	7.5	98	98	98	98	97	94	94	100	100	22765	17612	100	100	100	100	100	100	1168	395
Ef-Ro	34.7	99	99	100	100	99	98	98	96	92	-56	-4581	96	99	99	99	99	99	269	-100
Wb-On	30.9	99	100	100	100	100	100	100	100	100	1984	786	92	98	98	99	99	99	74	-117
Wb-Jb	31.5	98	98	97	97	95	91	91	82	64	1569	-1572	100	100	100	100	100	100	137	72
Wb-Cm	32.5	98	98	97	97	94	88	88	77	54	910	-1421	100	100	100	100	100	100	104	28
Wb-Mc	34.1	98	98	99	99	98	97	97	94	87	-7	-3125	95	98	99	99	99	99	56	-181
Wb-Nt	34.1	98	98	98	98	100	100	100	98	95	-185	-5859	97	99	99	99	99	99	92	-323
Wb-Tr	30.8	98	97	98	98	96	93	93	86	73	2495	-1198	100	100	100	100	100	100	-26	-183
Wb-Sh	6.7	98	99	98	98	96	93	93	100	100	22204	18062	100	100	100	100	100	100	1050	355
Wb-Ro	34.1	97	96	93	93	100	100	100	100	100	-866	-5159	97	99	99	99	99	99	297	-147
On-Jb	28.4	98	98	98	98	97	94	94	88	78	548	-3354	100	100	100	100	100	100	223	14
On-Cm	29.4	99	98	100	100	100	98	98	95	89	-94	-3194	95	98	99	99	99	99	205	-36
On-Mc	30.9	99	99	100	100	100	100	100	100	100	-1675	-4450	96	99	99	99	99	99	138	-249
On-Nt	30.9	98	99	98	98	100	100	100	100	100	-1870	-7022	97	99	99	99	99	100	146	-384
On-Tr	30.6	98	98	97	97	95	90	90	81	61	847	-2012	100	100	100	100	100	100	-44	-132
On-Sh	6.6	98	97	96	96	93	86	86	100	100	20266	16555	100	100	100	100	100	100	963	327
On-Ro	30.9	99	99	99	99	100	100	100	100	100	-2441	-7132	97	99	99	99	99	99	411	-219
Jb-Cm	33.6	98	96	93	93	86	73	73	57	15	179	-660	86	94	95	98	99	99	4	-43
Jb-Mc	32.2	98	98	98	98	97	95	95	91	83	1169	-4582	100	100	100	100	100	100	-9	-286
Jb-Nt	32.8	98	98	98	98	98	97	97	94	88	684	-7250	97	99	99	99	99	99	47	-422
Jb-Tr	28.2	98	98	98	98	97	95	95	91	83	3976	-2507	100	100	100	100	100	100	-127	-318
Jb-Sh	4.2	99	97	100	100	100	100	100	100	100	23466	21697	100	100	100	100	100	100	727	256
Jb-Ro	33.9	98	99	100	100	100	100	100	100	100	-1972	-4390	96	99	99	99	99	99	231	-176
Cm-Mc	33.2	98	98	98	98	97	95	95	90	81	1169	-3923	100	100	100	100	100	100	-9	-244
Cm-Nt	33.8	98	98	98	98	98	96	96	93	87	803	-6593	97	99	99	99	99	100	46	-381
Cm-Tr	29.2	97	98	98	98	97	95	95	91	82	3867	-1868	100	100	100	100	100	100	-72	-286
Cm-Sh	5.1	98	98	100	100	100	100	100	100	100	23430	20826	100	100	100	100	100	100	869	297
Cm-Ro	34.6	98	99	100	100	100	100	100	100	100	-1376	-4152	96	99	99	99	99	99	227	-150
Mc-Nt	38.3	98	97	98	98	96	92	92	87	80	209	-2737	94	98	98	99	99	99	42	-142
Mc-Tr	34.0	99	98	100	100	100	100	100	100	100	3407	1914	95	98	99	99	99	99	173	-179
Mc-Sh	10.2	98	98	98	98	98	96	96	100	100	23251	13962	100	100	100	100	100	100	1503	534
Mc-Ro	34.7	98	99	99	99	98	96	96	92	85	2279	-4612	100	100	100	100	100	100	306	28
Nt-Tr	34.0	98	97	96	96	100	100	100	100	100	5524	1864	97	99	99	99	99	99	296	-184
Nt-Sh	12.6	98	98	98	98	98	97	97	100	100	24241	10230	100	100	100	100	100	100	1764	675
Nt-Ro	35.3	98	98	98	98	98	97	97	94	88	5019	-4427	100	100	100	100	100	100	385	163
Tr-Sh	10.0	98	97	97	97	96	94	94	100	100	20075	12200	100	100	100	100	100	100	1315	453
Tr-Ro	30.7	98	99	99	99	100	100	100	100	99	-529	-7342	97	99	99	99	99	99	456	-120
Sh-Ro	6.7	98	99	98	98	100	100	100	100	100	-22750	-27344	100	100	100	100	100	100	-384	-1191